

ナイロン網地1反の空中重量

誌名	日本水産學會誌
ISSN	00215392
巻/号	533
掲載ページ	p. 385-388
発行年月	1987年3月

農林水産省 農林水産技術会議事務局筑波産学連携支援センター
Tsukuba Business-Academia Cooperation Support Center, Agriculture, Forestry and Fisheries Research Council
Secretariat



Practical Equations for the Weight in Air of One Strip of Nylon Netting*¹

Tadanobu Machii*² and Yukio Nose*³

(Accepted July 15, 1986)

Equations for the weight of netting are very important in designing fishing gears and in practical work, but there are very few studies on the subject. In this study, we developed equations for the weight in air of one strip of netting based on the Netting Weight Table. Whereas in the previous study, we derived them from a single mesh measurements. The material used is nylon multifilament and English knot. One strip of netting is equivalent to 100 fathoms' length with a depth of 100 meshes. Using the relations obtained in the previous study, we determined the constants for one strip of netting. The equations for the weight of netting (W) can be expressed with kg-cm units, as $W=n\{1+2/5(\sqrt{n}/L_m)\}$ in $3 \leq n \leq 51$ and $W=1.1 \cdot n \cdot \{1+2/5(\sqrt{n}/L_m)\}$ in $60 \leq n \leq 180$, where n is the number of yarns and L_m is the mesh size. Verifying the results, we found that the equations fitted very well with the values of the Netting Weight Table.

Equations for the weight of netting are acquiring greater importance in designing fishing gears and for practical use at field works.

Regarding this subject, we find only the studies of Nagamine¹⁾ and Miyamoto²⁾ for the weight in the air of natural fibers and Itaka³⁾ for the weight in the water of synthetic fibers.

In the previous study,⁴⁾ we determined the relation of the weight in the air for one strip of English knot nylon netting, which was derived from the relations of a single mesh and the measurements of netting.

The purpose of this study is to determine equations based on the relation of the previous study, from the Netting Weight Table and to verify the adequacy of the equations obtained in comparison with the values of the Netting Weight Table. We also discuss the lateral effect caused by the length of knot.

Materials and Methods

Although a netting is made with the same standard, there is a slight difference in the weight among fishing net manufactures. This difference depends on the twisting degree given for the legs

of netting in each manufacturer. In this study, we used the Netting Weight Table considering manufacture "A" as standard. The material is nylon multifilament, English knot, 210 denier and three strand twine from 3 to 180 yarns.

One strip of netting is defined in Japan by 100 "ken"^{*4} long and 100 meshes deep, but we used 100 fathoms' length, because this unit is recognized throughout the world. A single mesh consists of two legs and one knot, and the mesh size is the length of two legs and two knots. The units used are kilograms for weight and centimeters for length.

The weight in the air for one strip of nylon netting (W) was expressed by the relation in the previous study as

$$W = C_1 \cdot n + C_2 \left(\frac{n^{3/2}}{L_m} \right) \quad (1)$$

where L_m is the mesh size, n is the number of yarns, and C_1 and C_2 are the constants. Also, W , n and L_m are known variables taken from the Netting Weight Table.

From the equation (1), we can determine the constants C_1 and C_2 .

*¹ This paper was presented at the annual meeting of the Japanese Society of Scientific Fisheries, Sendai, Japan, October, 1984.

*² Department of Fishing Science & Technology, Tokyo University of Fisheries, Konan 4-5-7, Minato, Tokyo 108, Japan (町井紀之: 東京水産大学漁業生産学科).

*³ Department of Fisheries, Faculty of Agriculture, The University of Tokyo, Yayoi 1-1-1, Bunkyo, Tokyo 113, Japan (能勢幸雄: 東京大学農学部水産学科).

*⁴ 100 ken = 151.5 m, Japanese traditional fishing unit.

Results and Discussion

Determination of Equations and Their Verification

Table 1 shows the results obtained from the constants C_1 and C_2 for a given n . Both C_1 and C_2 should take theoretically the definite values. Though C_2 can be considered nearly as a unitary value, a tendency is observed in C_1 to increase for a given increase in n .

Consequently C_1 can not be treated as a unitary value capable of covering an overall range of n . In order to solve the practical side of this problem, we divided the range of n into two cases; *i.e.*, $3 \leq n \leq 51$ as a body netting and $60 \leq n \leq 180$ as a selvage netting.

In order to find the best values within the classified range of n , we carried out simulation tests for C_1 and C_2 to obtain high correlation values. The results obtained are $C_1=1.0$ and $C_2=0.40$ in $3 \leq n \leq 51$, and $C_1=1.1$ and $C_2=0.44$ in $60 \leq n \leq 180$.

From the constants obtained, the equations for the weight of one strip of netting can be expressed as follows;

$$W = n \cdot \left(1 + \frac{2}{5} \frac{\sqrt{n}}{L_m} \right) \quad (3 \leq n \leq 51) \quad (2)$$

and

$$W = 1.1 \cdot n \cdot \left(1 + \frac{2}{5} \frac{\sqrt{n}}{L_m} \right) \quad (60 \leq n \leq 180) \quad (3)$$

In order to verify the equations, we calculated with the equation (2) four examples of L_m from 3.49 to 24.1 cm in $3 \leq n \leq 51$, and with the equation (3) five examples from 4.45 to 8.89 cm in $60 \leq n \leq 180$. About the range of L_m , the former

Table 1. Constants obtained from the Netting Weight Table of Nylon*

n	L_m (cm)		No. of data	Constants	
	Min.	Max.		C_1	C_2
3	0.953	24.1	49	0.955	0.384
6	"	"	"	0.947	0.406
9	"	"	"	0.972	0.396
12	"	"	"	0.991	0.434
15	1.27	"	48	0.984	0.406
18	1.59	"	47	0.999	0.411
21	"	"	"	0.945	0.502
24	1.90	"	46	0.956	0.476
27	2.22	"	45	0.978	0.459
30	"	"	"	0.982	0.456
36	"	"	"	0.984	0.491
45	2.86	"	43	1.07	0.421
51	3.49	"	41	1.06	0.455
60	"	"	"	1.06	0.507
75	"	"	"	1.01	0.481
90	"	"	"	1.14	0.465
120	5.08	"	36	1.14	0.429
150	"	"	"	1.16	0.390
180	"	"	"	1.21	0.372

* 100 fathoms' long and 100 meshes deep in the case of English knot.

covers all the body netting, the latter includes practically the selvage netting range.

The comparison of the values between the Netting Weight Table (*Tab.*) and the calculation by the equations (*Cal.*) are shown in Table 2, where R (%) ($\{(Cal. - Tab.) / Tab.\} \times 100$) is the error by *Cal.* as compared to *Tab.*

Regarding R in Table 2, in $3 \leq n \leq 51$, when n is a fixed value, R seems to vary inversely according to the increment of L_m , and when L_m is a fixed value, R increases at both extremes of n . In $60 \leq n \leq 180$, the difference of R can not be clearly observed depending on L_m (n : fixed value).

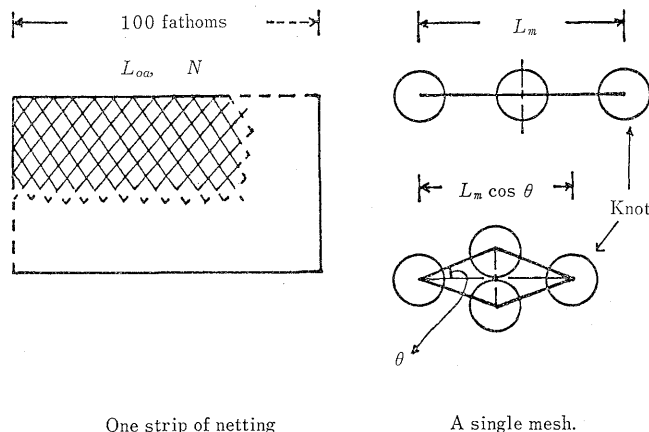


Fig. 1. Lateral effect caused by the length of knots. L_{0a} : Lateral stretched length of 100 fathoms, N : Total lateral number of mesh within 100 fathoms, L_m : Mesh size, and θ : Angle based on the lateral effect.

Table 2. Comparisons of the weight in the air for one strip of netting* between Netting Weight Table values and calculated values

L_m	Body Netting						Selvage Netting								
	3.49 cm 1 3/8"		7.62 cm 3"		11.7 cm 4 5/8"		24.1 cm 9 1/2"		6.35 cm 2 1/2"		6.99 cm 2 3/4"		8.89 cm 3 1/2"		
n	Tab. kg	Cal. kg	R %	Tab. kg	Cal. kg	R %	Tab. kg	Cal. kg	R %	Tab. kg	Cal. kg	R %	Tab. kg	Cal. kg	R %
3	3.48	3.60	3.36	3.14	3.27	4.17	3.03	3.18	4.78	2.85	3.09	8.36			
6	7.35	7.68	4.47	6.41	6.71	4.73	6.25	6.55	4.85	6.06	6.24	2.97			
9	11.87	12.09	1.86	10.00	10.42	4.13	9.67	9.92	2.61	9.36	9.45	0.90			
12	16.99	16.76	-1.37	14.16	14.18	0.13	13.43	13.42	-0.13	12.71	12.69	-0.20			
15	21.44	21.66	0.98	17.87	18.05	1.00	16.89	16.98	0.53	15.84	15.96	0.81			
18	27.08	26.75	-1.23	21.92	22.01	0.41	20.83	20.60	-1.08	19.09	19.27	0.90			
21	32.87	32.02	-2.59	25.80	26.05	0.98	24.19	24.28	0.38	22.44	22.60	0.68			
24	38.44	37.47	-2.53	29.68	30.17	1.67	28.09	28.01	-0.31	25.97	25.95	-0.08			
27	44.79	43.07	-3.84	34.27	34.37	0.27	32.22	31.78	-1.37	29.45	29.33	-0.43			
30	50.88	48.82	-4.04	38.68	38.63	0.15	36.14	35.60	-1.51	32.94	32.72	-0.45			
36	66.19	60.74	-8.23	48.18	47.34	-1.75	45.08	43.36	-3.81	39.68	39.58	-0.24			
45	85.51	79.58	-6.94	63.46	60.85	-4.12	59.38	55.29	-6.90	51.98	50.00	-1.92			
51	104.2	92.72	-11.0	74.65	70.12	-6.07	68.43	63.41	-7.34	58.32	57.04	-2.19			
L_m	4.45 cm 1 3/4"		5.08 cm 2"		6.35 cm 2 1/2"		6.99 cm 2 3/4"		8.89 cm 3 1/2"						
n	Tab. kg	Cal. kg	R %	Tab. kg	Cal. kg	R %	Tab. kg	Cal. kg	R %	Tab. kg	Cal. kg	R %	Tab. kg	Cal. kg	R %
60	117.2	112.0	-4.39	108.6	106.3	-2.15	99.6	98.6	-1.37	96.5	95.3	-1.21	88.8	89.0	0.21
72	139.0	139.7	0.53	129.6	132.1	1.94	117.7	121.5	3.40	114.4	117.7	2.88	103.4	109.4	5.81
75	145.9	146.8	0.60	135.7	138.8	2.23	123.9	127.5	2.95	120.5	123.4	2.44	109.0	114.7	5.17
90	189.8	183.5	-3.30	171.7	173.0	0.76	165.0	158.2	-4.13	160.5	152.8	-4.79	148.4	141.3	-4.82
96				186.7	187.1	0.20	178.3	170.8	-4.20	173.4	164.9	-4.91	160.6	152.2	-5.27
120				245.4	245.9	0.19	223.9	223.1	-0.38	217.8	214.8	-1.38	201.5	197.1	-2.18
150				312.2	324.1	3.82	284.5	292.3	2.75	276.9	280.7	1.37	256.3	255.9	-0.13
180				390.9	407.2	4.16	356.7	365.3	2.42	345.0	350.1	0.91	320.9	317.8	-0.95

* 100 fathoms' long and 100 meshes deep in the case of English knot nylon netting

As a result, the equations (2) and (3) fitted very well with the values of the Netting Weight Table.

Lateral Effect Caused by the Length of Knots

When we assume that the total lateral number of mesh within 100 fathoms (N) and the mesh size (L_m) are known variable, there are two criteria in the lateral stretched length of one strip of netting (L_{oa}) as shown in Fig. 1.

One is the length (L_{oa1}) from the criteria in the previous study, without consideration to lateral effect caused by the length of knots (called here the lateral effect). The other is the length (L_{oa2}) from the Netting Weight Table in this study, taking into account the lateral effect.

So, the relation between L_{oa2} and L_{oa1} can be written as

$$\frac{L_{oa2}}{L_{oa1}} = \cos \theta \tag{4}$$

where θ is the angle based on the lateral effect. As shown by the equation (4), when taking L_{oa1} as standard, L_{oa2} is shorter than L_{oa1} with the increment of θ .

On the other hand, when we assume that L_{oa} and L_m are known variables, there are also two criteria in the N as shown in Fig. 1.

One is the total lateral number of mesh (N_1), from the criteria in the previous study, without consideration to the lateral effect. The other is the total lateral number of mesh (N_2), from the Netting Weight Table in this study, with consideration to the lateral effect.

So, the relation between N_1 and N_2 can be written as

$$\frac{N_2}{N_1} = \frac{1}{\cos \theta} \tag{5}$$

The equation (5) shows, when taking N_1 as standard, N_2 is larger than N_1 with the increment of θ .

From the previous study W could be expressed as

$$W = n \cdot \left(1 + \frac{1}{3} \frac{\sqrt{n}}{L_m} \right) \quad (6 \leq n \leq 180) \tag{6}$$

In order to verify the lateral effect, we compared difference of values between the *Tab.* and *Cal.* by the calculation of the equation (6) as shown in Table 3, where E (%) ($\{(Tab. - Cal.) / Cal.\} \times 100$) is the lateral effect.

The length of one knot (L_k) is proportional to \sqrt{n} , and L_k / L_m is proportional to $\sin \theta$. However, the lateral effect is clearly found in Table 3,

Table 3. Lateral effect E (%) caused by the length of knots for one strip of netting*

Body Netting					
L_m	3.49 cm	7.62 cm	11.7 cm	24.1 cm	
n	1 3/8"	4"	4 5/8"	9 1/2"	
3	-0.52	-2.64	-3.69	-7.29	
6	-0.67	-3.54	-2.66	-2.25	
9	2.51	-1.78	-1.04	-0.10	
12	6.38	2.47	1.86	1.07	
15	4.34	1.87	1.41	0.23	
18	7.06	2.71	3.24	0.18	
21	8.87	2.34	1.89	0.49	
24	9.11	1.84	2.71	1.34	
27	10.9	3.42	3.95	1.76	
30	11.4	4.02	4.21	2.07	
36	16.9	6.01	6.94	1.78	
45	15.8	9.03	10.8	5.70	
51	21.5	11.5	11.5	4.07	

Selvage Netting					
L_m	4.45 cm	5.08 cm	6.35 cm	6.99 cm	8.89 cm
n	1 3/4"	2"	2 1/2"	2 3/4"	3 1/2"
60	23.6	20.0	18.0	17.4	14.7
72	18.0	15.6	13.1	13.1	9.0
75	18.0	15.4	13.6	13.7	9.7
90	23.3	17.6	22.4	22.8	21.6
96		18.4	22.6	23.1	22.3
120		19.0	18.5	19.2	19.0
150		15.4	15.4	16.5	17.1
180		15.5	16.3	16.9	18.6

* 100 fathoms' long and 100 meshes deep in the case of English knot nylon netting

according to the increment of n and/or with the decrement of L_m .

As mentioned above, there is the difference in the criteria between the previous study and this study. This is the reason why the constant C_1 could not be treated as a unitary value in this study.

In conclusion, we can apply the equations (2) and (3) for full scale net making, including the lateral effect for the calculations. The equation (6) can be used for the calculation necessary to make model nets, excluding the lateral effect in the calculations.

References

- 1) T. Nagamine: *Saishin Gyorōgaku* (Modern Fishing Arts), Kōsei-kaku, Tokyo, 1932, pp. 43-45.
- 2) H. Miyamoto: *Teichiami Gyoron* (Stationary Fishing Gears), Kawade shobō, Tokyo, 1954, pp. 93-96.
- 3) Y. Iitaka: *Nippon Suisan Gakkaishi*, **24**, 620-621 (1958).
- 4) T. Machii and Y. Nose: *Nippon Suisan Gakkaishi*, **53**, 381-383 (1987).